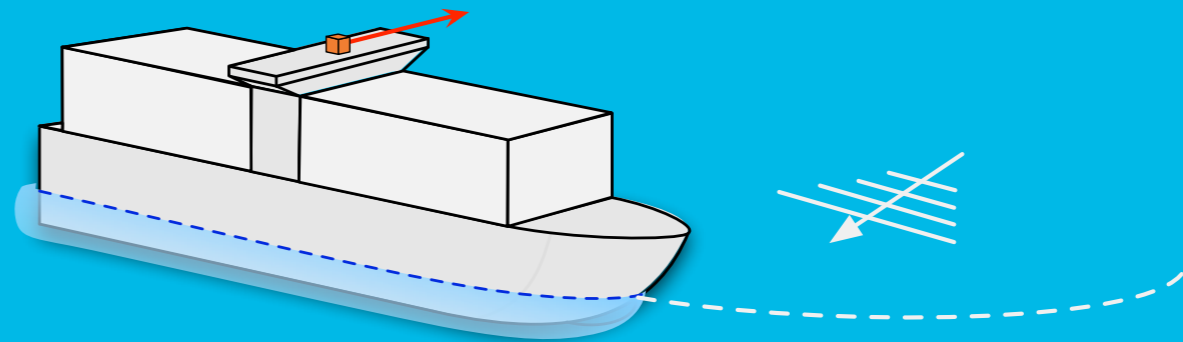


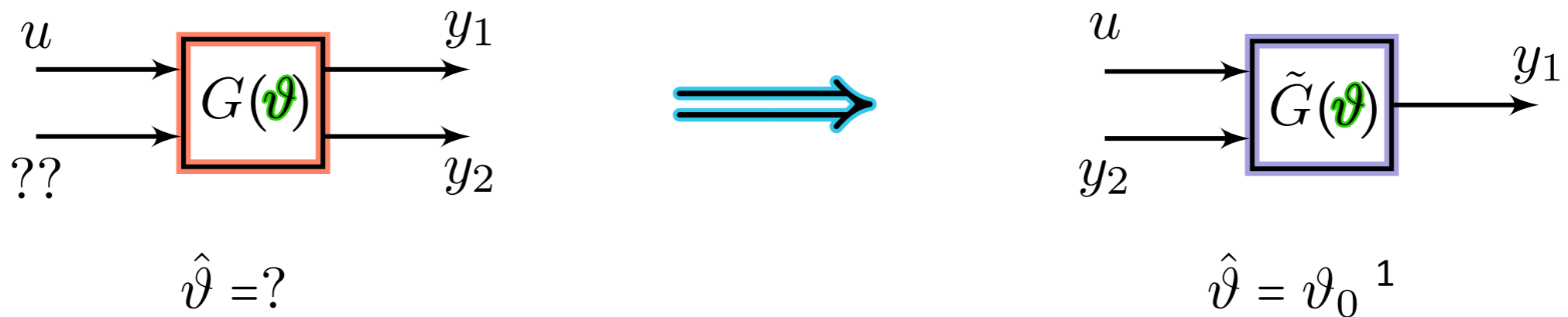
# Identification of Systems with Unknown Inputs Using Indirect Input Measurements

Jonas Linder and Martin Enqvist



# Overview

A framework for **systematically reformulating** a **model with unknown inputs** into a **model with known inputs** that can be used to estimate the **desired dynamics**

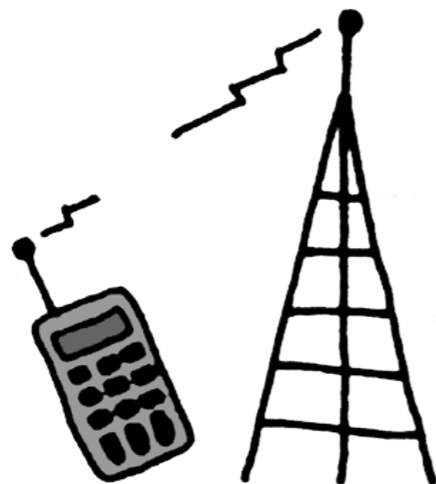
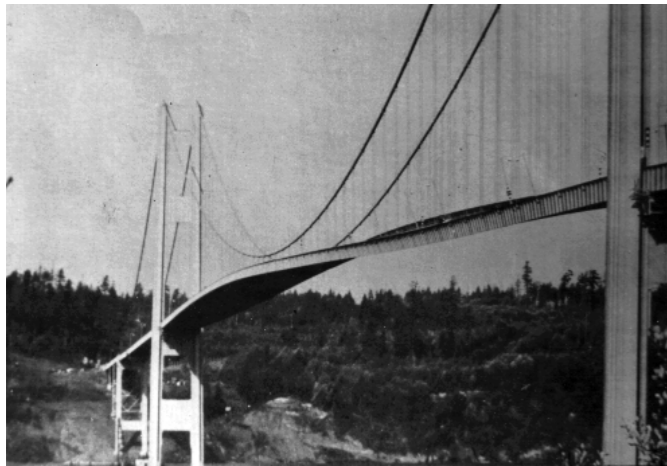


<sup>1</sup> Sometimes :)

# Motivation - Systems with unknown inputs

## Examples

- Robotics – varying payload
- Automotive industry – slope of road
- Marine applications – wind and wave
- Bridges and planes – vibration in structure
- Telecommunication – unknown data and channel

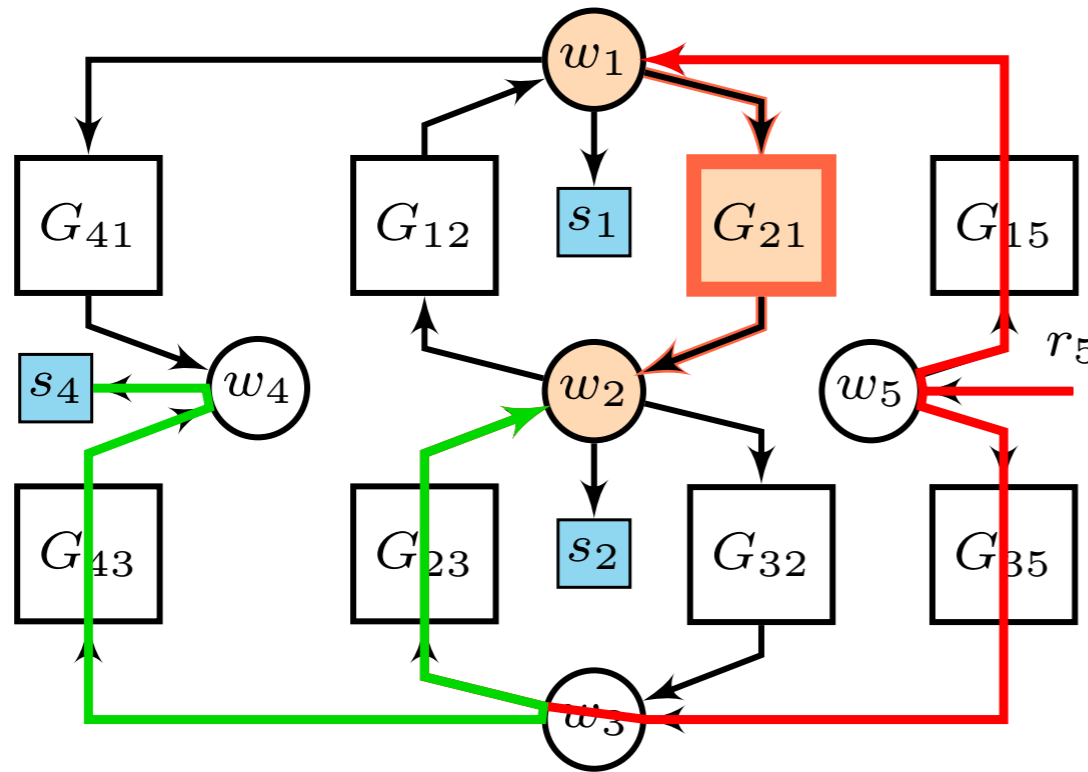


Indirect framework

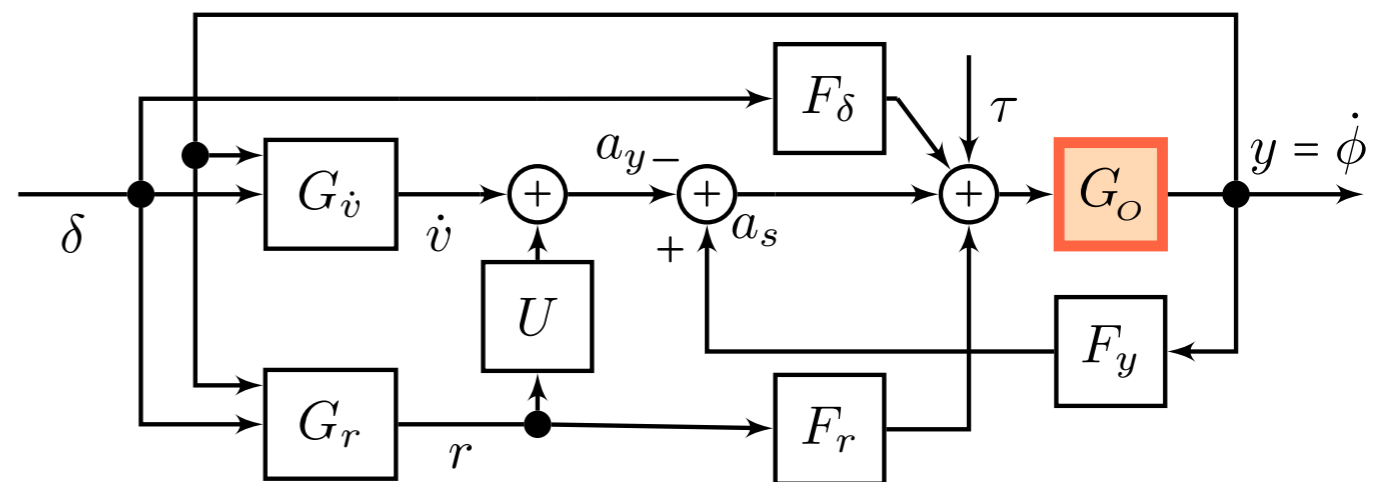
## Remedies for unknown inputs

1. Neglect or partially mitigate
2. Measure – EIV
3. Eliminate – sensor-to-sensor
4. Assume – time-series, blind identification

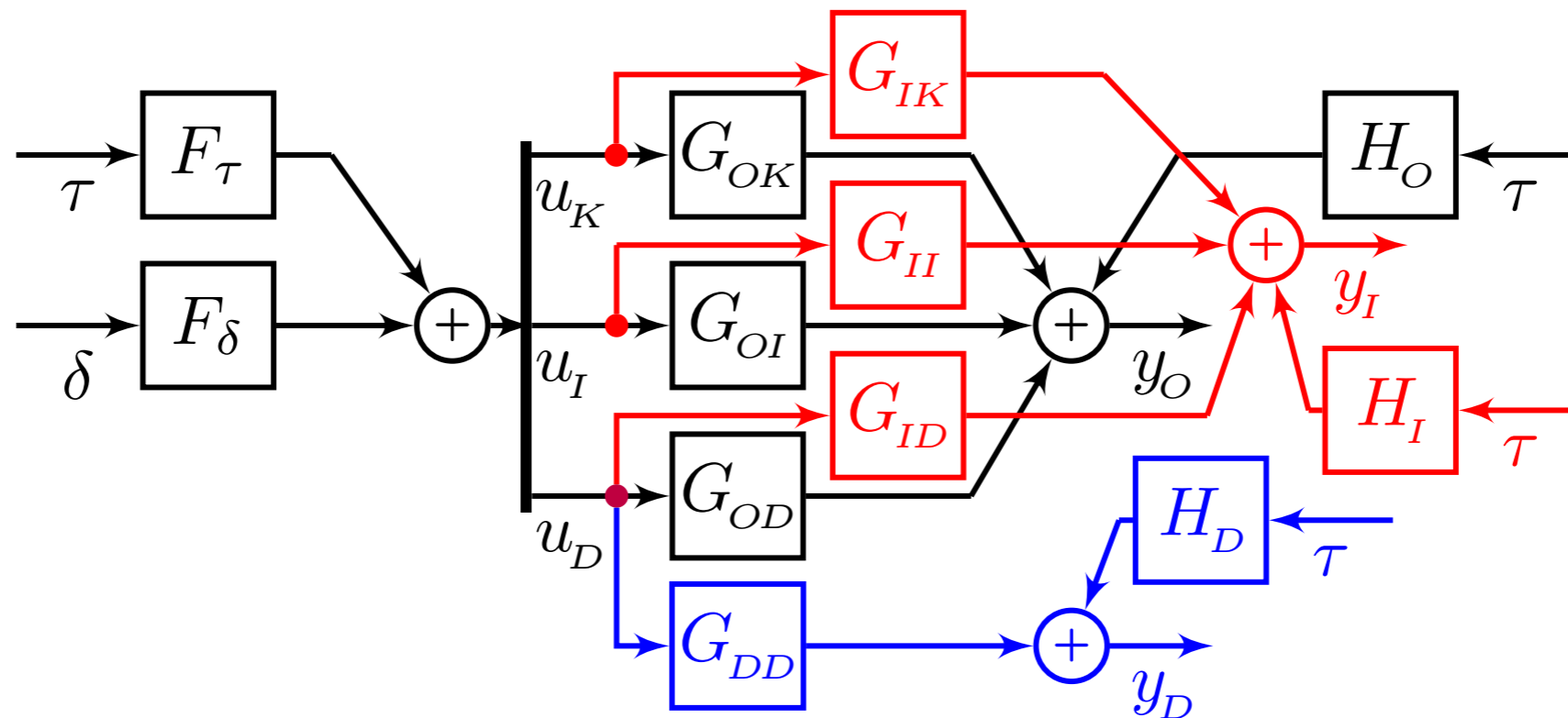
# Motivation - Illustrative example



- Complete model intractable
- Estimate part of system
- Limited measurements  $s_x$
- Correlation  $\implies$  bias
- Indirect input measurements
- Unconventional networks



# Problem formulation



- Estimate the MIMO transfer function  $G_O(p)$  from

$$y_O = G_O(p)u + H_O(p)\tau \quad \text{and} \quad u = F_\delta\delta + F_\tau\tau$$

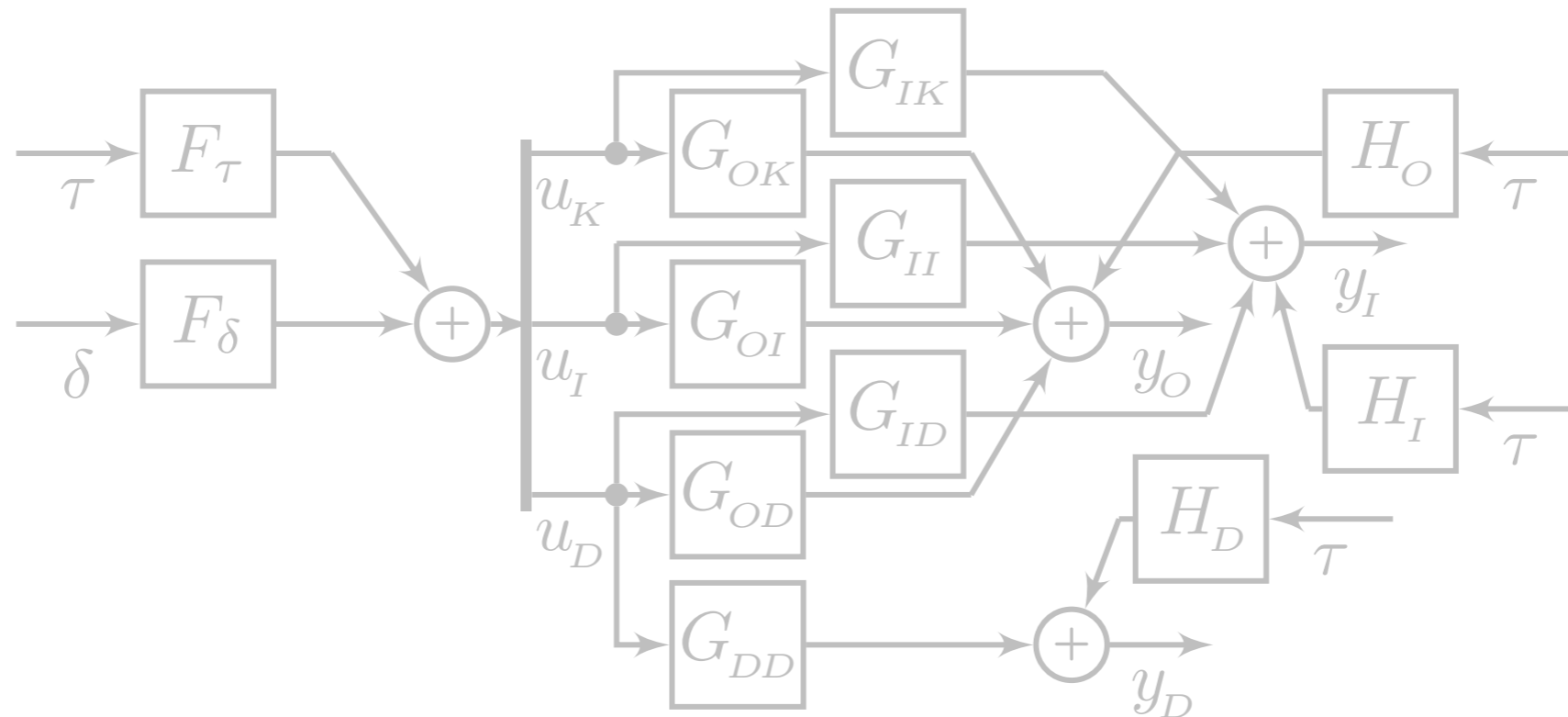
- The input is assumed to be (partially) unknown

$$u = \begin{bmatrix} u_K \\ u_I \\ u_D \end{bmatrix} \left. \begin{array}{l} \text{(exactly) known} \\ \text{unknown} \end{array} \right\}$$

- Extend model with the **direct**- and **indirect** input measurements

$$\begin{bmatrix} y_O \\ y_I \\ y_D \end{bmatrix} = \begin{bmatrix} G_{OK} & G_{OI} & G_{OD} \\ G_{IK} & G_{II} & G_{ID} \\ 0 & 0 & G_{DD} \end{bmatrix} \begin{bmatrix} u_K \\ u_I \\ u_D \end{bmatrix} + \begin{bmatrix} H_O \\ H_I \\ H_D \end{bmatrix} \tau$$

# Problem formulation - Indirect model



- **Idea:** Eliminate unknown input using **algebraic manipulation**
- **Assumption:** There exist filters  $f_{DD}$  and  $f_{II}$ , such that  $f_{DD}G_{DD} = I$  and  $f_{II}G_{II} = I$
- Solve for  $G_{DD}u_D$  and  $G_{II}u_I$  and apply filters

$$u_D = f_{DD} [y_D - H_D\tau] \quad u_I = f_{II} [y_I - G_{IK}u_K - G_{ID}u_D - H_I\tau]$$

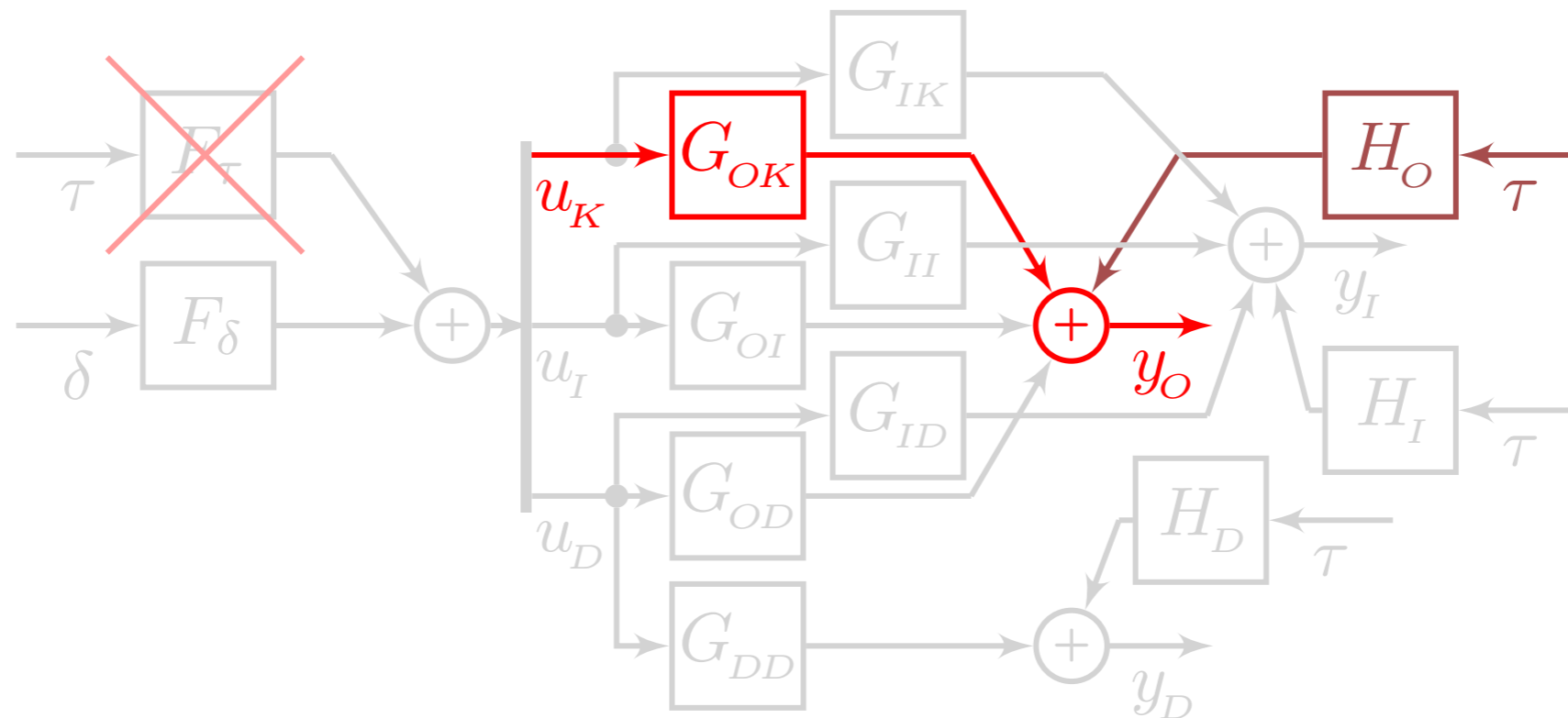
- The indirect model

$$y_O = [\tilde{G}_{OK}u_K + \tilde{G}_{OI}y_I + \tilde{G}_{OD}y_D] + \bar{\tau} = \tilde{G}_O\tilde{u} + \bar{\tau}$$

- Extend model with the **direct**- and **indirect** input measurements

$$\begin{bmatrix} y_O \\ y_I \\ y_D \end{bmatrix} = \begin{bmatrix} G_{OK} & G_{OI} & G_{OD} \\ G_{IK} & G_{II} & G_{ID} \\ 0 & 0 & G_{DD} \end{bmatrix} \begin{bmatrix} u_K \\ u_I \\ u_D \end{bmatrix} + \begin{bmatrix} H_O \\ H_I \\ H_D \end{bmatrix} \tau$$

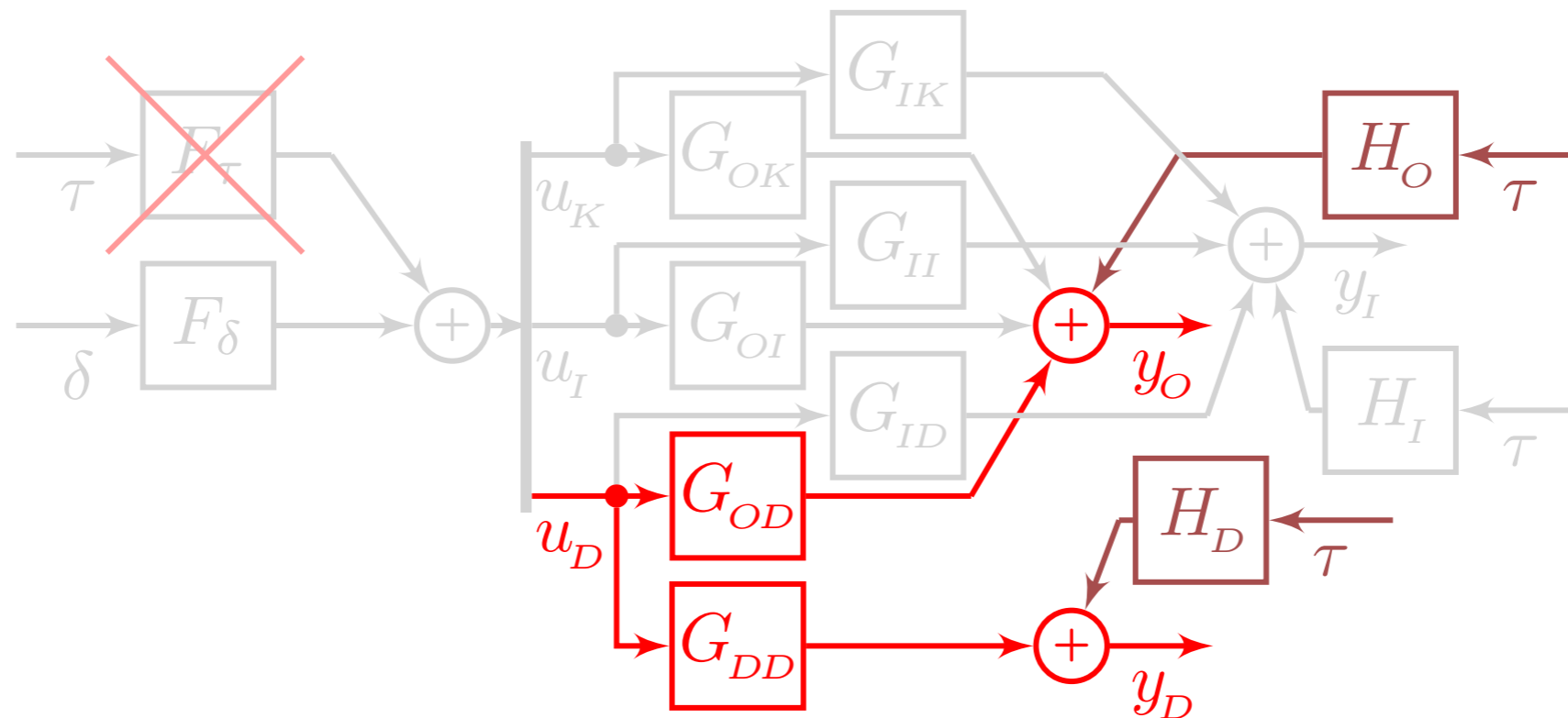
# Connection to previous work - Open-loop configuration



$$y_O = [G_{OK} - G_{OI}G_{II}^{-1}G_{IK}]u_K + [G_{OI}G_{II}^{-1}]y_I + [G_{OD} - G_{OI}G_{II}^{-1}G_{ID}]G_{DD}^{-1}y_D + \bar{\tau}$$

- Input *uncorrelated* with the process disturbance, i.e.  $F_\tau = 0$ 
  - All inputs known: Classic open-loop

# Connection to previous work - Open-loop configuration

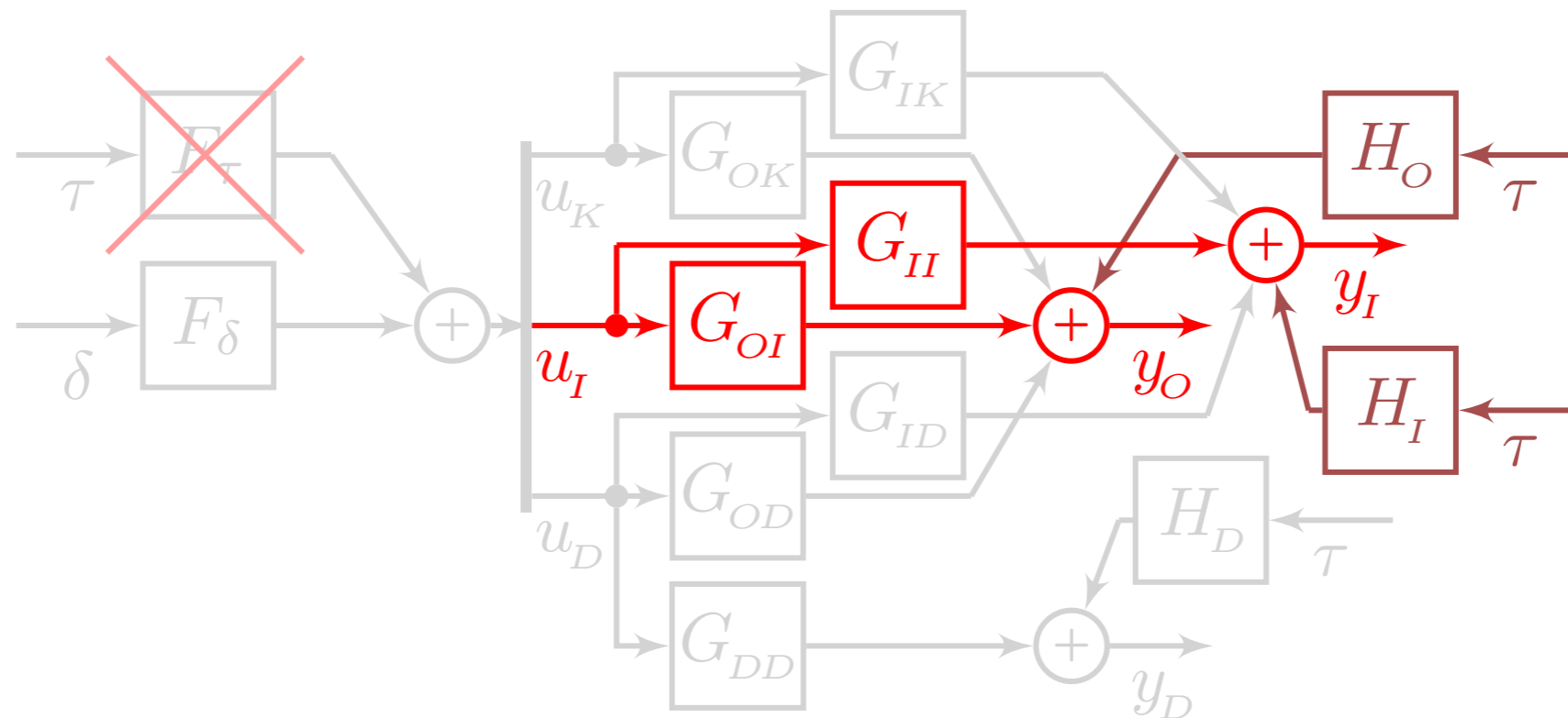


$$y_O = [G_{OK} - G_{OI}G_{II}^{-1}G_{IK}]u_K + [G_{OI}G_{II}^{-1}]y_I + [G_{OD} - G_{OI}G_{II}^{-1}G_{ID}]G_{DD}^{-1}y_D + \bar{\tau}$$

- Input *uncorrelated* with the process disturbance, i.e.  $F_\tau = 0$ 
  - All inputs known: Classic open-loop
  - All inputs directly measured: Classic errors-in-variable ( $G_{DD} = I$  and  $e_D = H_D\tau$ )



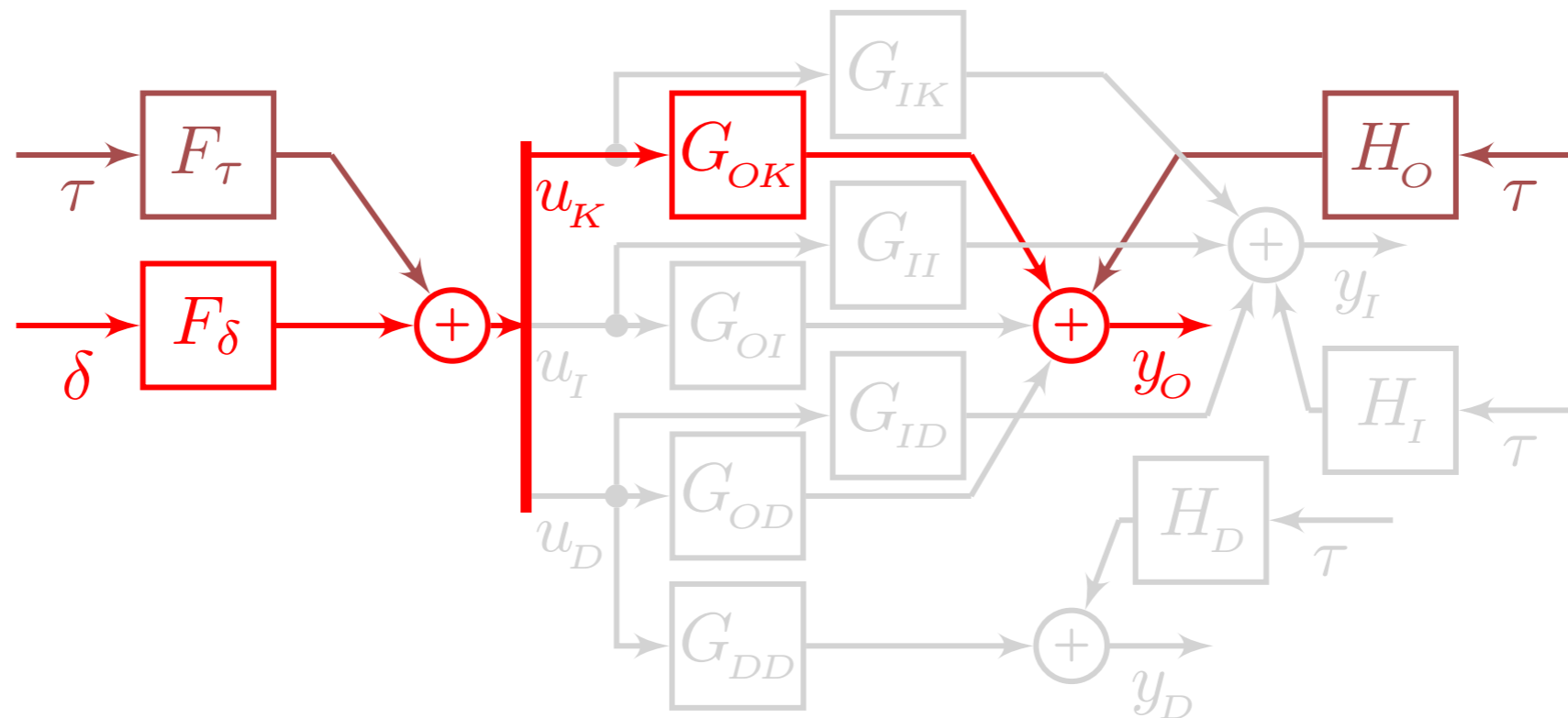
# Connection to previous work - Open-loop configuration



$$y_O = [G_{OK} - G_{OI}G_{II}^{-1}G_{IK}]u_K + [G_{OI}G_{II}^{-1}]y_I + [G_{OD} - G_{OI}G_{II}^{-1}G_{ID}]G_{DD}^{-1}y_D + \bar{\tau}$$

- Input *uncorrelated* with the process disturbance, i.e.  $F_\tau = 0$ 
  - All inputs known: Classic open-loop
  - All inputs directly measured: Classic errors-in-variable ( $G_{DD} = I$  and  $e_D = H_D\tau$ )
  - All inputs indirectly measured: Sensor-to-sensor system identification problem

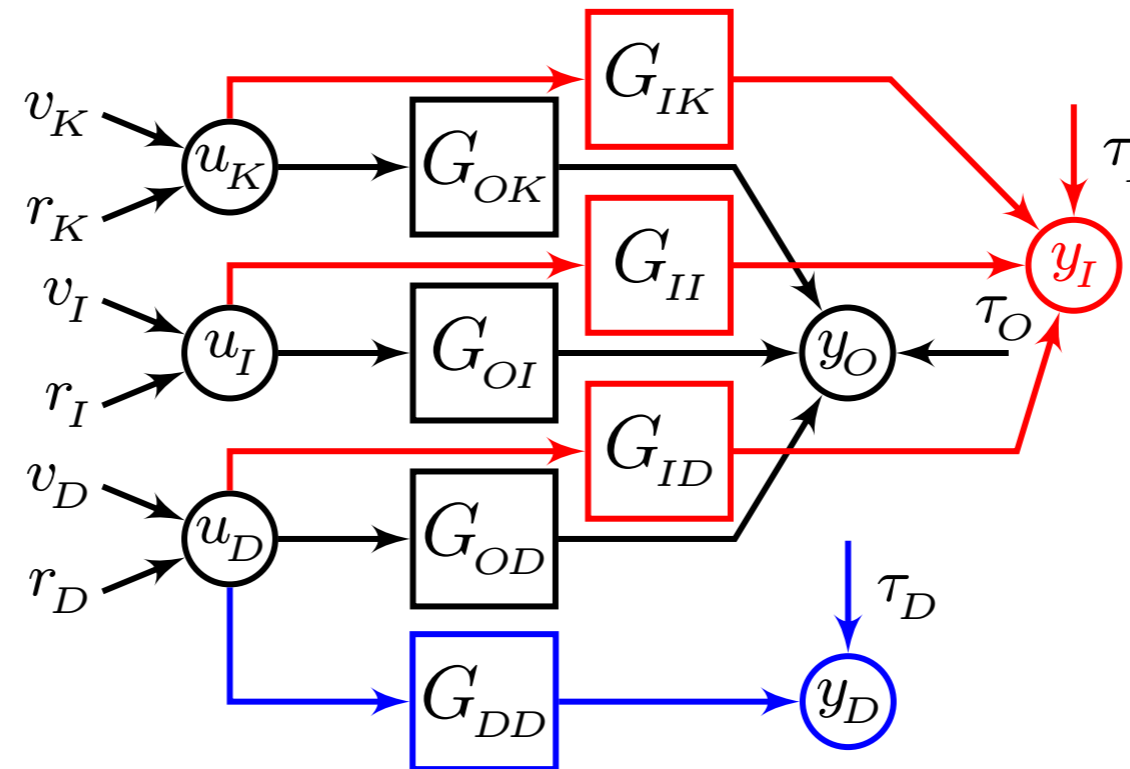
# Connection to previous work - Closed-loop configuration



$$y_O = [G_{OK} - G_{OI}G_{II}^{-1}G_{IK}]u_K + [G_{OI}G_{II}^{-1}]y_I + [G_{OD} - G_{OI}G_{II}^{-1}G_{ID}]G_{DD}^{-1}y_D + \bar{\tau}$$

- Input *uncorrelated* with the process disturbance, i.e.  $F_\tau = 0$ 
  - All inputs known: Classic open-loop
  - All inputs directly measured: Classic errors-in-variable ( $G_{DD} = I$  and  $e_D = H_D\tau$ )
  - All inputs indirectly measured: Sensor-to-sensor system identification problem
- Input *correlated* with the process disturbance, i.e.  $F_\tau \neq 0$ 
  - All inputs known: Classic closed-loop

# Connection to previous work - Closed-loop configuration



$$y_O = [G_{OK} - G_{OI}G_{II}^{-1}G_{IK}]u_K + [G_{OI}G_{II}^{-1}]y_I + [G_{OD} - G_{OI}G_{II}^{-1}G_{ID}]G_{DD}^{-1}y_D + \bar{\tau}$$

- Input *correlated* with the process disturbance, i.e.  $F_\tau \neq 0$  (continued)
  - Dynamic networks where the notation  $v = F_\tau \tau$  and  $r = F_\delta \delta$  is used

## Generality of the Indirect Framework

- Both  $F_\tau$  and  $F_\delta$  can be full matrices (allows correlation between external signals)
- The indirect model “flips the arrows” to utilize the input measurements

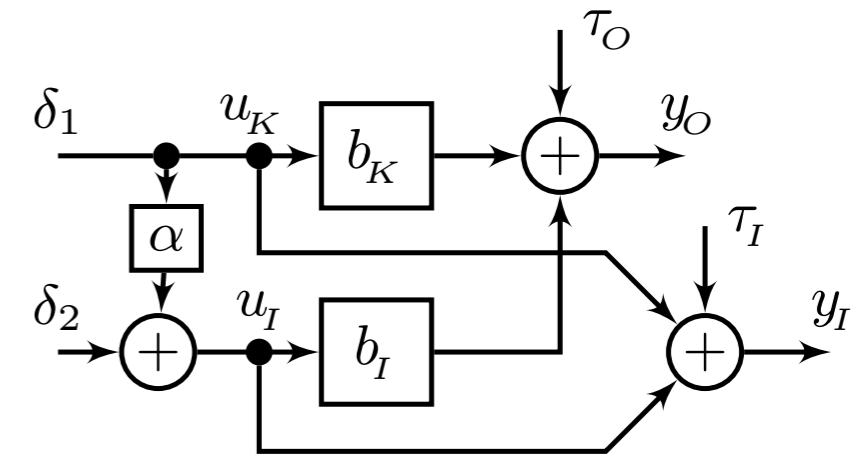
# Benefits of the framework

Why is it necessary or beneficial to include an input?

- Identifiability – can both be gained and lost
- Consistency and Variance

# Benefits of the framework - Consistency & variance

- An input can typically be neglected without affecting the consistency if it is independent of the remaining inputs.
- It is beneficial to use the input measurement if the signal-to-noise ratio is high.



## Example

True system

$$y_O = b_K u_K + b_I u_I + \tau_O$$

$$y_I = u_K + u_I + \tau_I$$

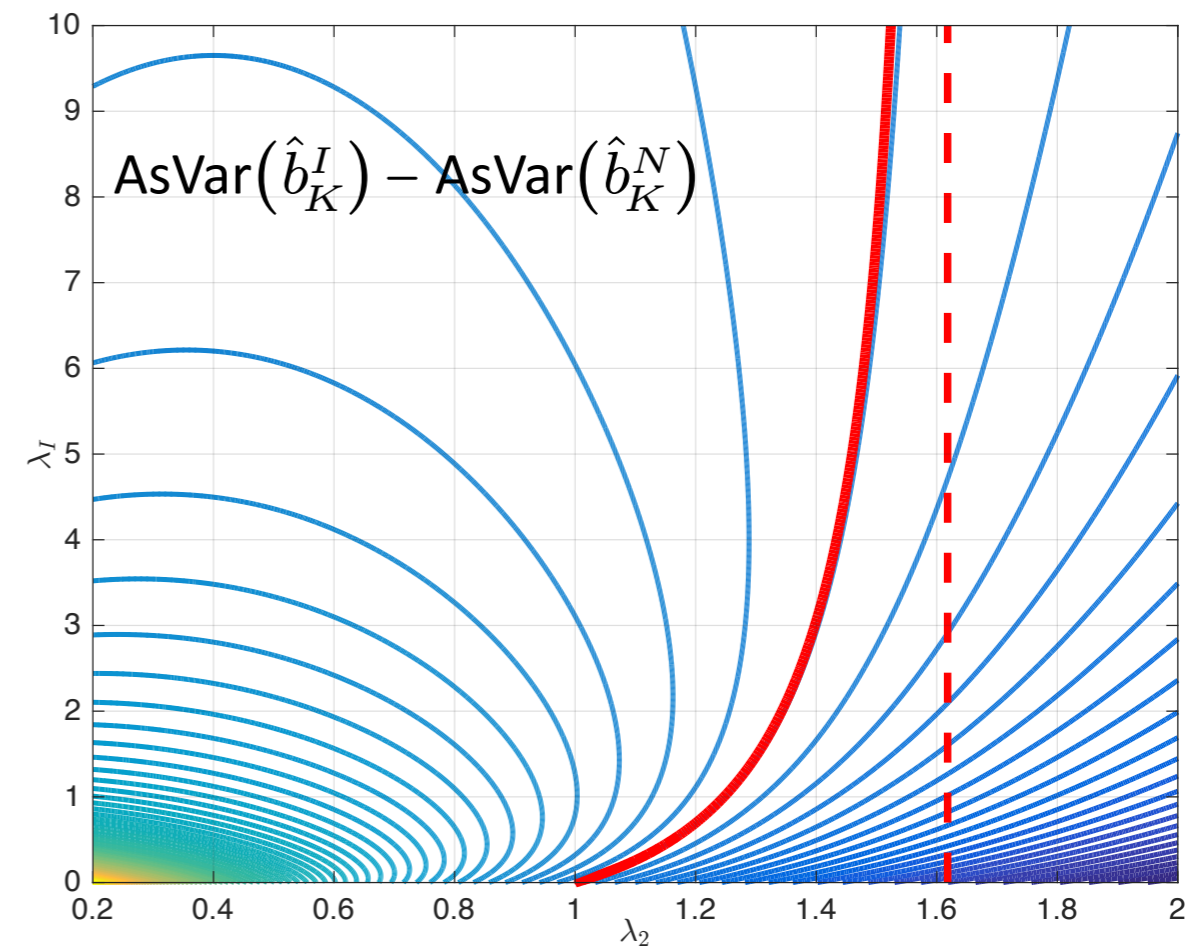
where we are interested in  $b_K$ .

Predictor with neglected input

$$\hat{y}_O = \hat{b}_K^N u_K \Rightarrow b_K^* = b_K + \alpha b_I$$

Predictor with using input measurement

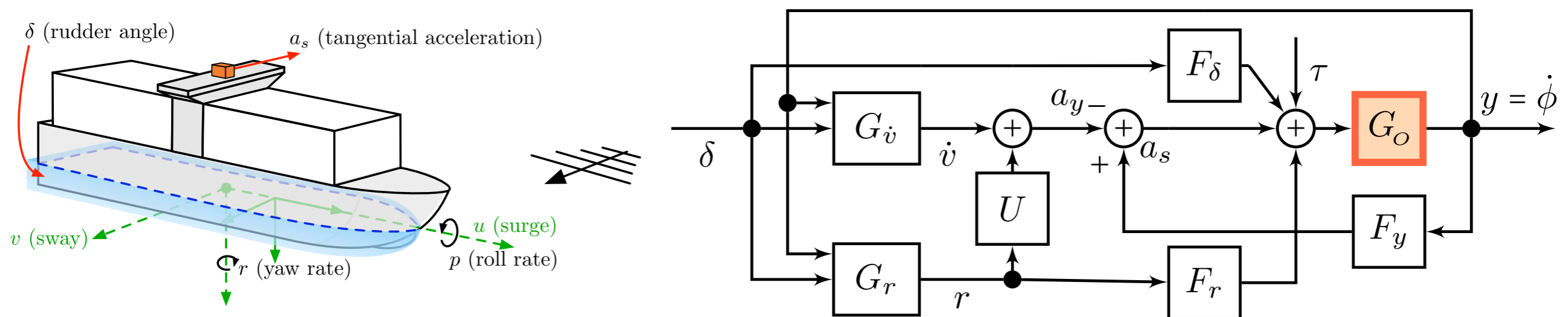
$$\hat{y}_O = (\hat{b}_K^I - \hat{b}_I) u_K + \hat{b}_I y_I \Rightarrow b_K^* = b_K + \alpha b_I \frac{\lambda_I}{\lambda_2 + \lambda_I}$$



# Example



# Example



- The roll subsystem can be described by

$$(A_x + Mz_g^2)\ddot{\phi} = -(k + Mgz_g)\phi - d\dot{\phi} + (K_{\dot{v}} + Mz_g)\dot{v} + (K_{ur} + Mz_g)Ur + K_{\delta}\delta + \tau$$

- Only measure the motion with an inertial measurement unit (IMU) (and the rudder angle)

$$y_{1,t} = \dot{\phi}_t + b_{1,t} + e_{1,t} - \text{roll rate}$$

$$y_{2,t} = a_{s,t} + b_{2,t} + e_{2,t} - \text{tangential acceleration}$$

$$y_{3,t} = -r_t + b_{3,t} + e_{3,t} - \text{yaw rate}$$

$$y_{4,t} = \delta_t + e_{4,t} - \text{rudder angle}$$

- The signal  $\dot{v}$  is unknown but indirectly measured by the IMU

$$a_s = z_s\ddot{\phi} + g\phi - \dot{v} - Ur$$

- The indirect model is given by

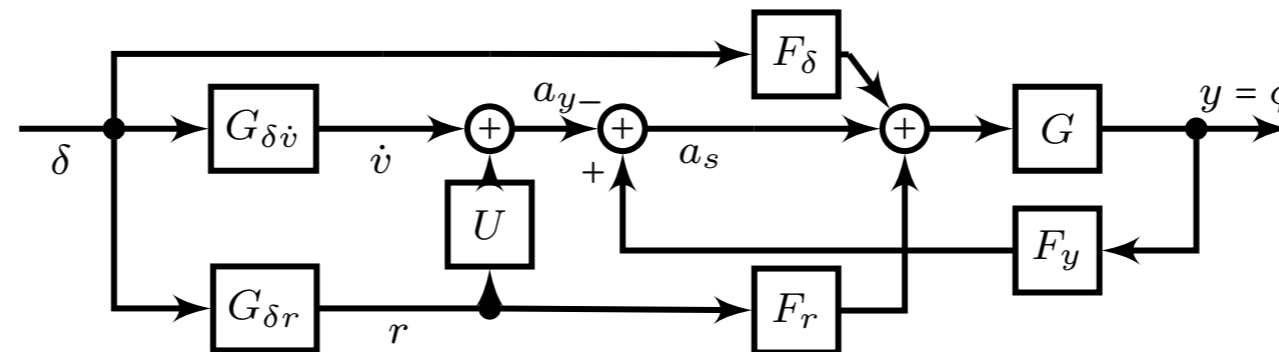
$$(A_x + Mz_g(z_g - z_s))\ddot{\phi} = -(k - K_{\dot{v}}g)\phi - d\dot{\phi} - (K_{\dot{v}} + Mz_g)a_s + K_r r + K_{\delta}\delta + \tau$$

# Example - Estimation

- An instrumental variable method is a correlation based approach, in principle

$$\frac{1}{N} \sum_{t=1}^N \underbrace{\zeta_t (y_t - \varphi_t^T \vartheta)}_{\varepsilon_t} = 0$$

- The instruments  $\zeta_t$  should be
  - correlated with the motion induced by the rudder
  - uncorrelated with the motion induced by the disturbance
- The optimal instruments would be the noise-free signals (intractable)
- The instruments are created by simulating the signals using the rudder signal

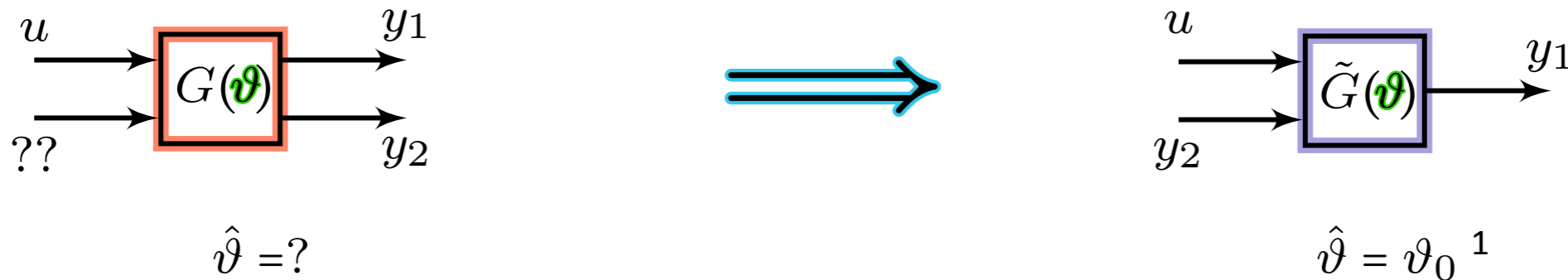


 J. Linder et. al. Modeling for IMU-based Online Estimation of Ship's Mass and Center of Mass  
In *Proceedings of the 10th IFAC Conference on Manoeuvring and Control of Marine Craft*, Copenhagen, 2015.

 J. Linder et. al. Online Estimation of Ship's Mass and Center of Mass Using Inertial Measurements  
In *Proceedings of the 10th IFAC Conference on Manoeuvring and Control of Marine Craft*, Copenhagen, 2015.



# Conclusions



- Unknown input exist in many engineering applications
- A framework using indirect input measurements
- Several already existing models are recovered as special cases
- The benefits of using the framework

<sup>1</sup> Sometimes :)

# Identification of Systems with Unknown Inputs Using Indirect Input Measurements

Jonas Linder and Martin Enqvist

